



Laser induced shockwave droplet breakup dynamics

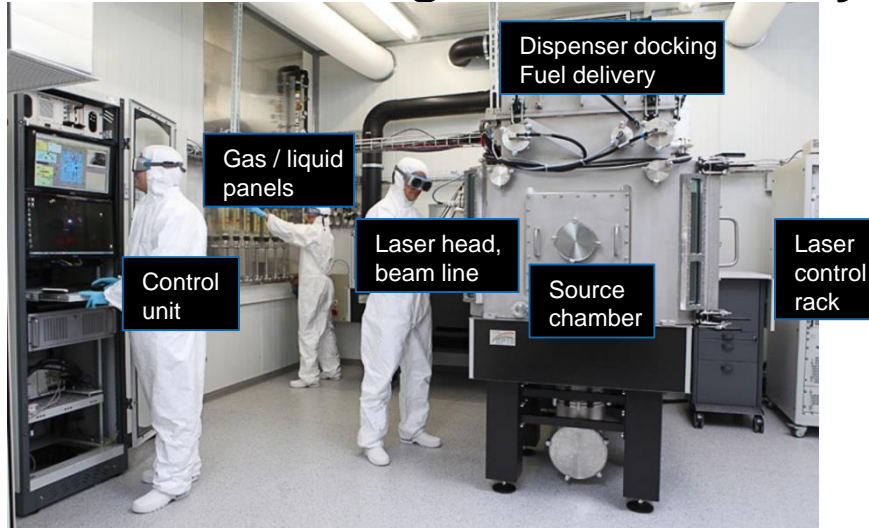
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Presentation Outline

- Neutral Cluster Dynamics
- Model Description
 - VOF Geometry and Numerical Methods
 - Initial Conditions
- Simulations Results Overview
- Droplet Fragmentation Analytical Model
- Comparison with Experimental Results
- Conclusions

ALPS II EUV Light Source – Key Numbers

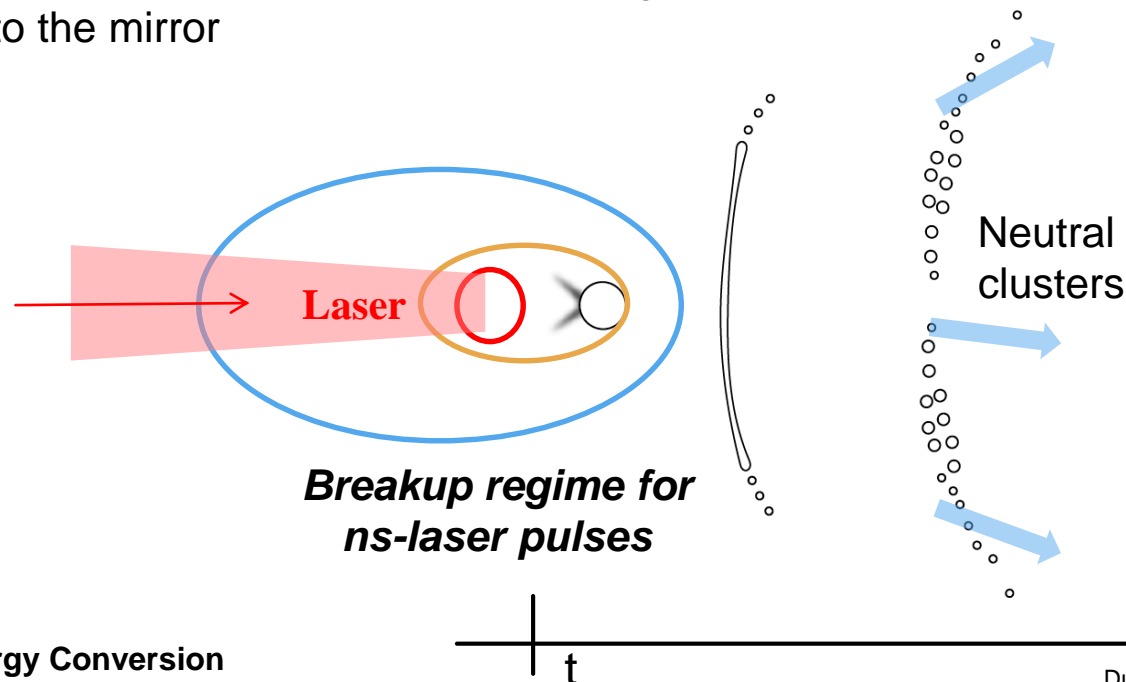


Parameters	Value
Laser power on target (W)	1400
Laser frequency (kHz)	>8
Laser focal spot size (μm)	70 (FWHM)
EUV source size (μm)	60 (FWHM)
Conversion efficiency (%)	>1%
Source power at the source (W)	>12
Source brightness ($\text{W}/\text{mm}^2\text{sr}$)	350

- Driven by DPSS Nd:YAG laser (average power of 1.4 kW, 1.064 μm , 8-20 kHz).
- 6th generation in-house droplet dispenser >30 μm tin droplet generation for hours of operation.
- Droplet tracking system with laser triggering on individual droplets enables droplet-laser alignment within <10% of droplet diameter.
- Full diagnostic including in-band energy monitors and out-of-band spectroscopy
- Debris mitigated grazing incidence collector, including clean IF module with imaging capability.
- Compatible with various collector configurations

Work goal is to predict size and distribution of neutral clusters

- Majority of droplet and plasma debris mass are *neutral clusters*
 - Neutral clusters are the liquid droplet fragments ejected away from the plasma region
 - This work is focused on predicting the formation and distribution of neutral clusters
 - Unablated droplet is flattened into a liquid sheet and then breaks into small droplets
 - Plasma formation and expansion occurs within 30-40 ns, liquid deformation timescale is on the order of $> 1\mu\text{s}$
- Splashes can affect ML collector mirror through direct impact and/or bouncing on one surface onto the mirror



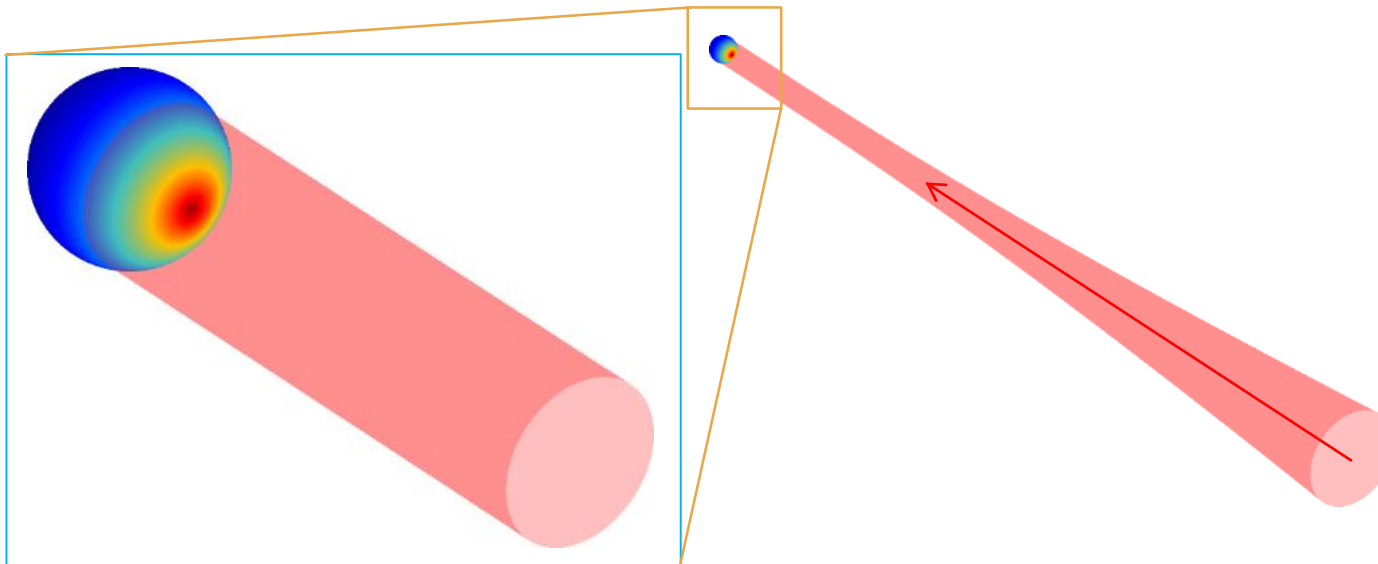
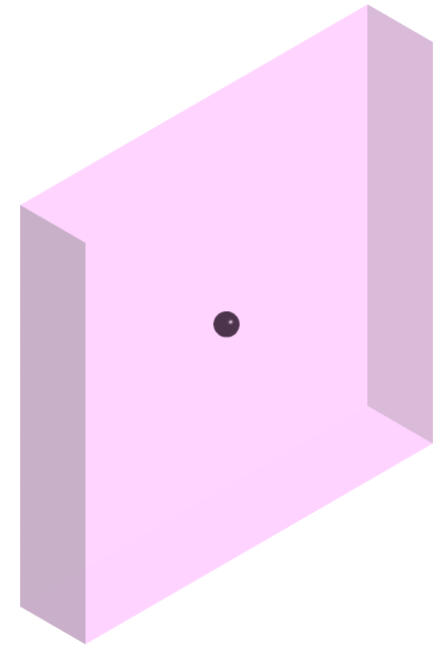
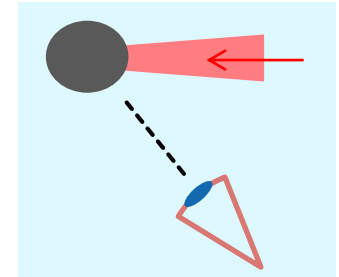
Volume of Fluid CFD Model with Moving Domain

Simulation Setup

- Run in Fluent 18.0
- Volume of Fluid (VOF) model with Coupled Level-Set Method
- Geo-reconstruct scheme

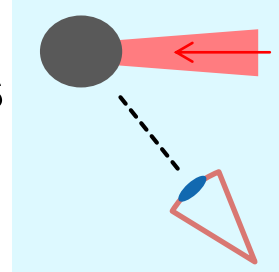
Domain Geometry

- Moving Reference Frame
- Droplet initialized in center of the rectangular cuboid domain
- Cuboid wall boundary conditions set to constant pressure outlet



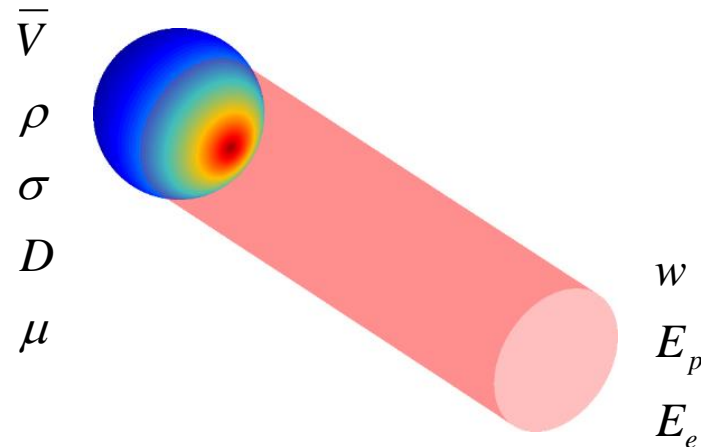
Six cases were simulated over a range of pulse energies

- $We = 120 - 15'000$
- $Re = 5'900 - 62'000$
- $E_e^* = 78 - 800$
- $\log_{10}(E_p^*) = 5.4 - 7.5$
- $w/D = 0.41 - 0.97$



$$E_e^* = E_e \sqrt{\frac{\rho D^3}{\sigma^3}} \quad E_p^* = \frac{E_p}{D^2 \sigma}$$

- $w = 1/e^2$ beam waist radius
- E_p = laser pulse energy
- E_e = laser pulse irradiance
- \bar{V} = mean radial neutral cluster velocity
- ρ = density
- D = droplet diameter
- ρ = density
- σ = surface tension
- μ = dynamic viscosity



Expanding ablated material transfers momentum to remaining droplet fluid*

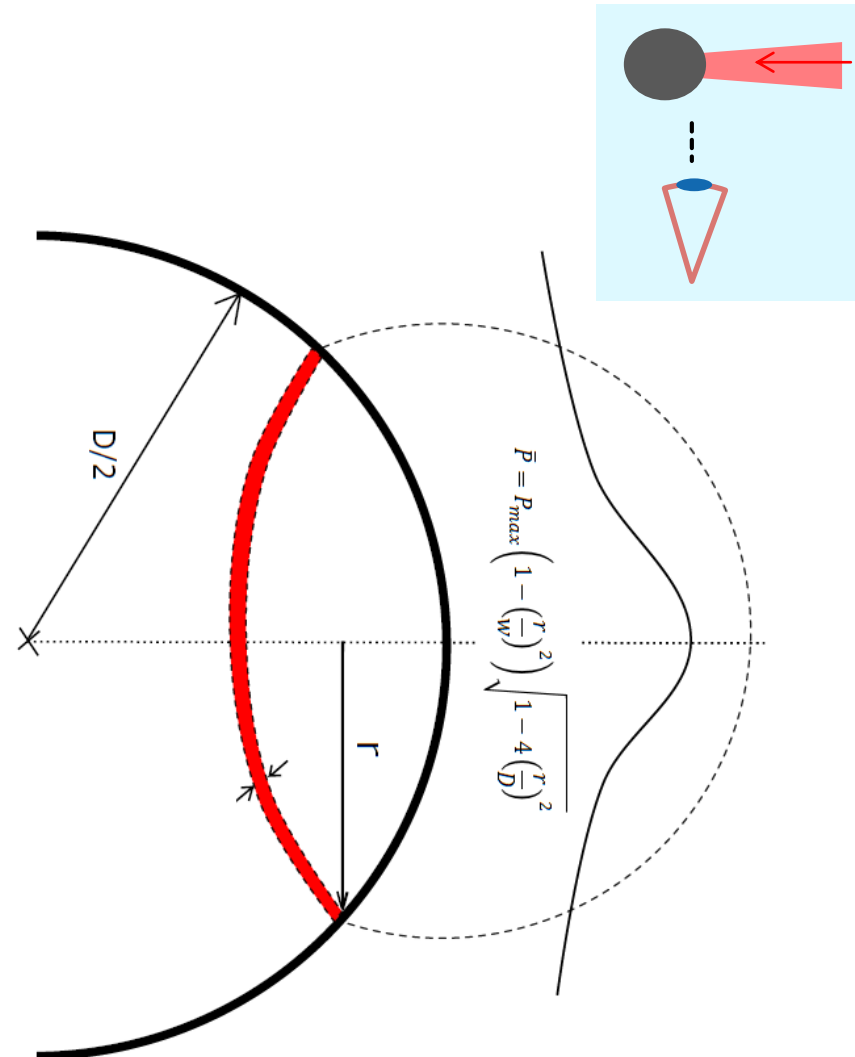
- Peak pressure on droplet surface:

$$\bar{P} = P_{max} \left(1 - \left(\frac{r}{w} \right)^2 \right) \sqrt{1 - 4 \left(\frac{r}{D} \right)^2}$$

- Ablation pressure**:

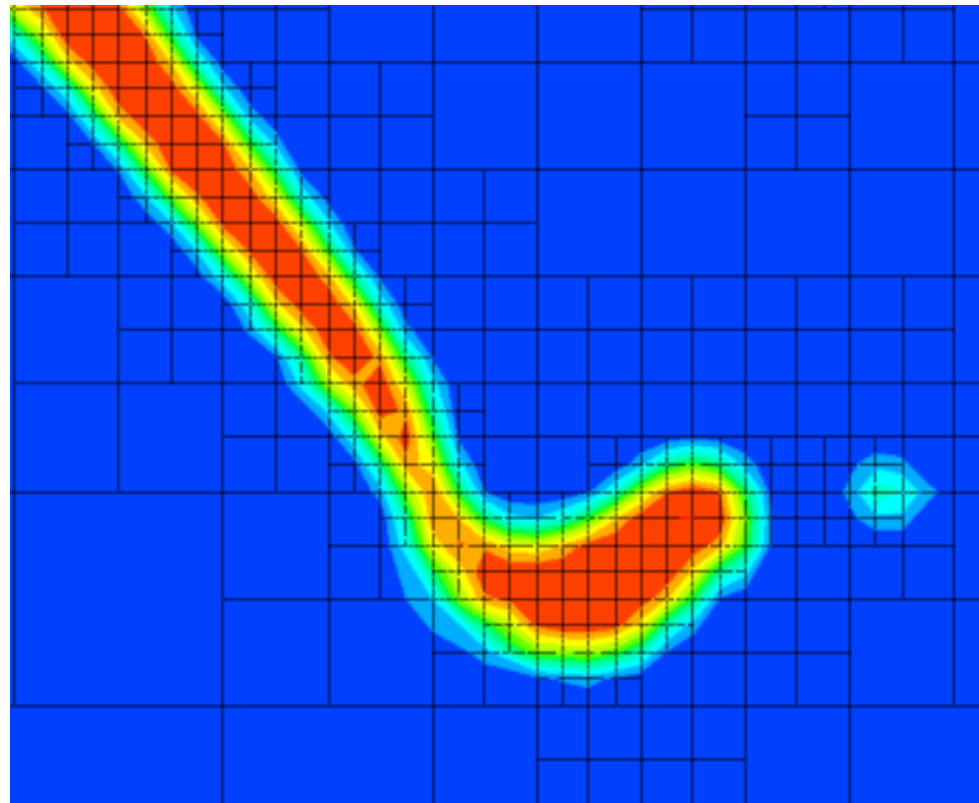
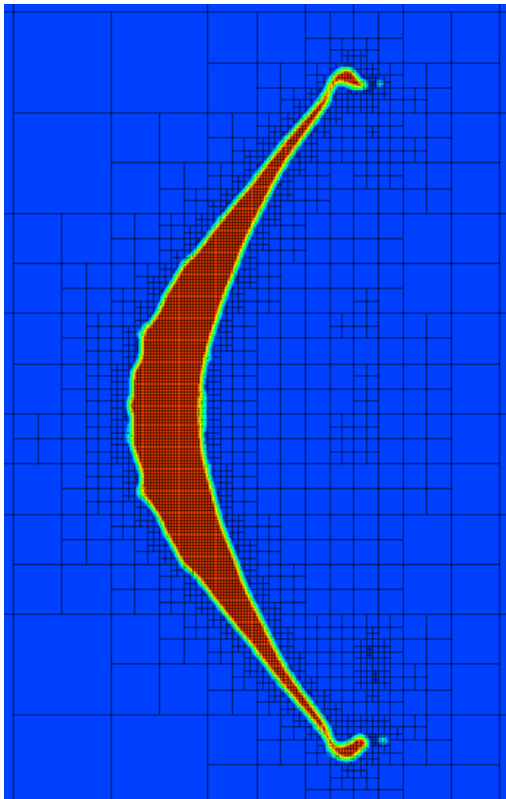
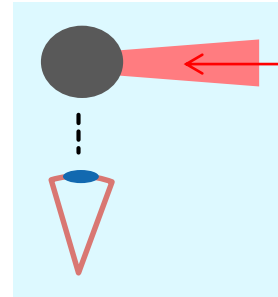
$$P_{max} \cong 8 \cdot I_0^{0.7} / \left(1 + \frac{l_{ac}^{(0)} \sin(\theta)}{w} \tau_p^{0.9} I_0^{0.3} \right)^{1.4}$$

- $l_{ac}^{(0)}$ = nominal critical surface distance
- $w = 1/e^2$ beam waist radius
- P_{max} = peak ablation pressure
- I_0 = Laser Irradiance
- θ = ray convergence angle
- τ_p = laser pulse duration
- D = droplet diameter



High resolution meshing adapted around droplet fluid

- Adaptive Meshing used in order to reduce computational costs of large domain/fluid volume ratio $O(3)$
- Mesh is adapted after every time step
- Mesh refined for cells with droplet fluid



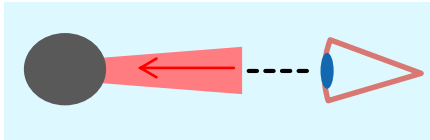
Simulated droplet fragments as expanding sheet

Simulations run until the fragments ceased dividing

$$\tau_D = \sqrt{\frac{\rho D^3}{6\sigma}}$$

$$t^* = \frac{t}{\tau_D}$$

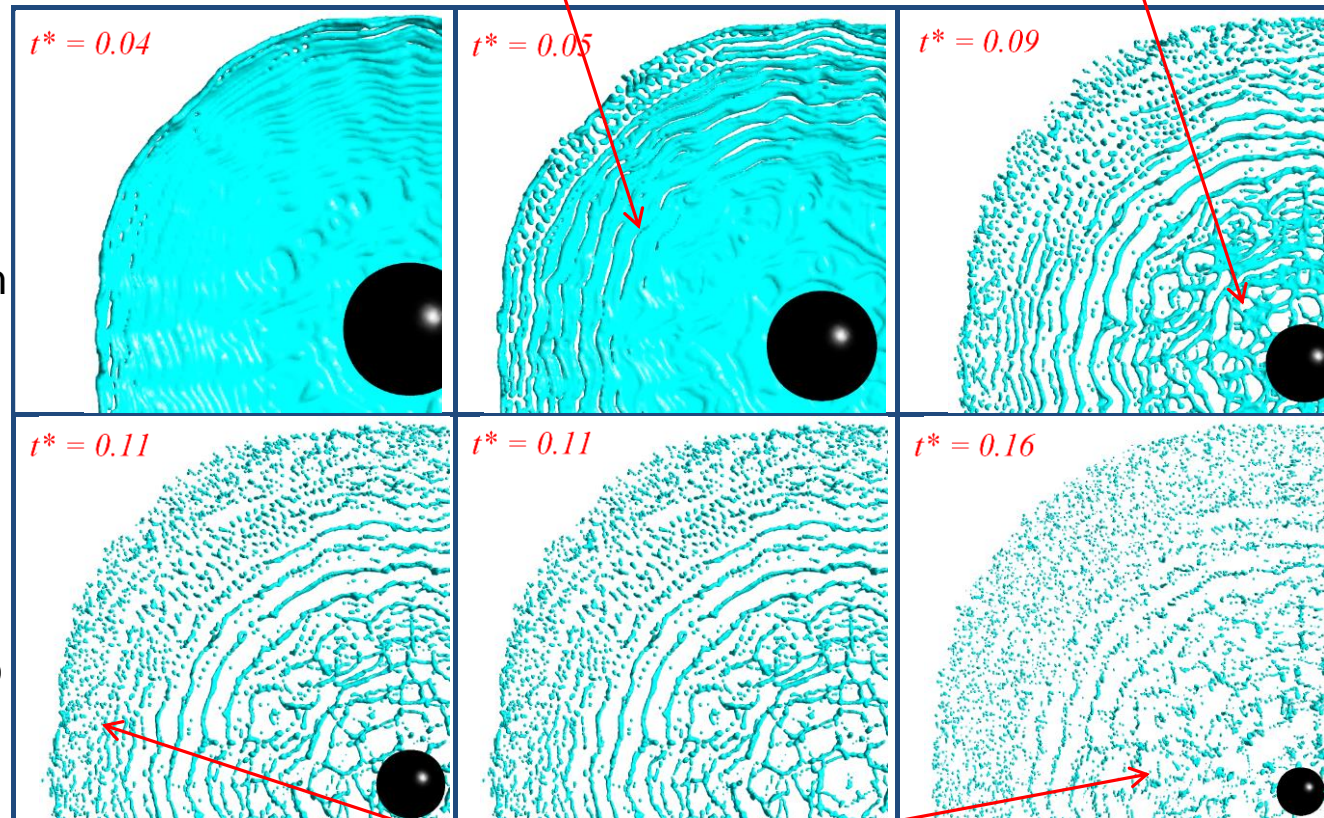
Breakup Radius



Growing Perforations

Breakup Dynamics

- 1) Droplet flattens into a circular sheet
- 2) Ligaments separate from rim at critical radius
- 3) Ligaments breakup into fragments
- 4) Smaller ligaments ejected first
- 5) Center of sheet grows holes, which expand into ligaments that fragment

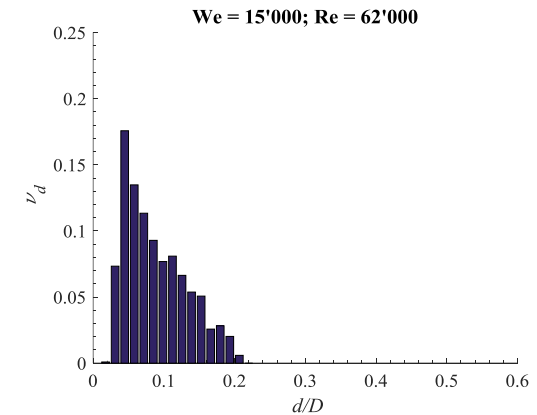
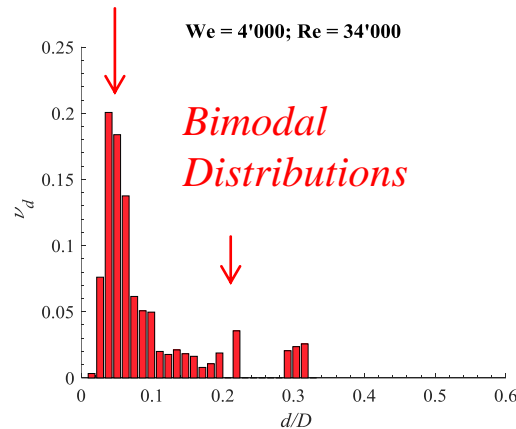
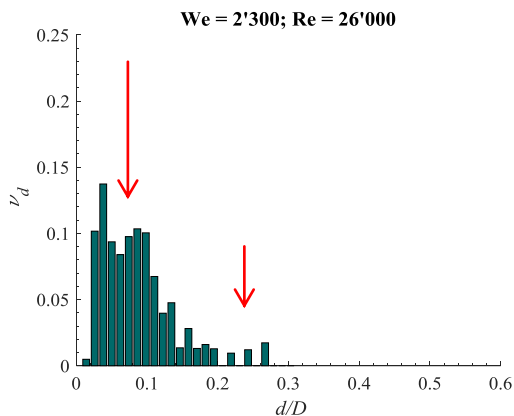
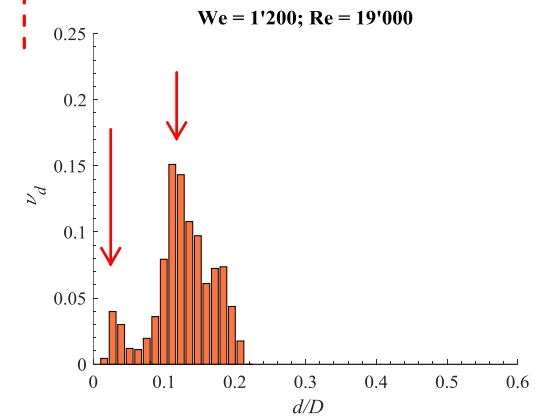
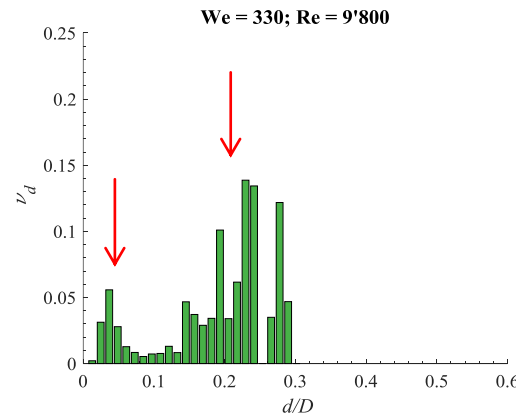
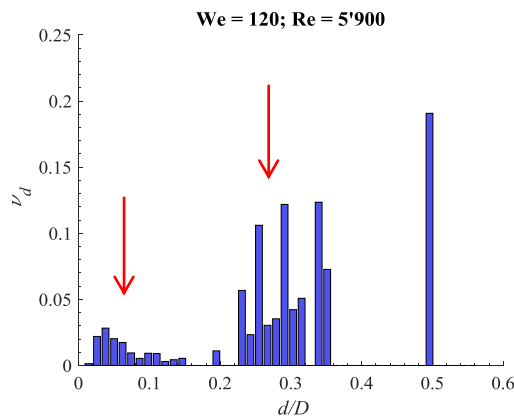


Ligaments fragment into droplets

Simulated fragment mass distributions show two breakup regimes

- Fragments sorted by size, position and velocity for analysis
- Splash regime is dominant at $We > 1'000$

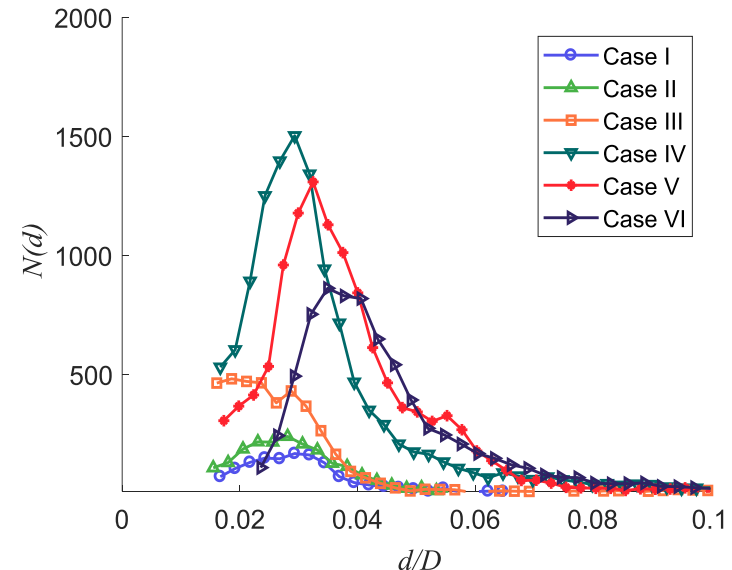
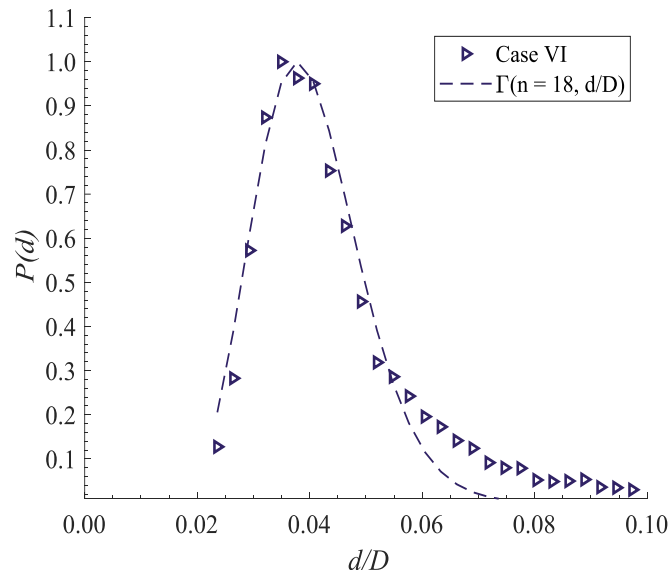
$We > 1'000$



Simulated fragment size distributions indicate fragmentation from splashing rather than viscous sheet retraction

- Fragment size probability distribution functions (PDF) for fragment size for each case with a 95% confidence interval.
- PDF's for all cases emulate a *gamma* distribution*
- Parameter n calculated from the stretch rate γ^{**}
- Number of fragments increase with Weber number until fragment volume limit reached
- Mean fragment diameter does not vary substantially with We indicating splashing, a process dominated by inertial/geometric influences**
- Broader size spectrum for higher We indicates lower stretch rate of original ligaments

$$\Gamma(n, x = d/d_\Gamma) = \frac{n^n}{\Gamma(n)} x^{n-1} \cdot e^{-nx}$$



Model of rim breakup matches well with CFD simulations

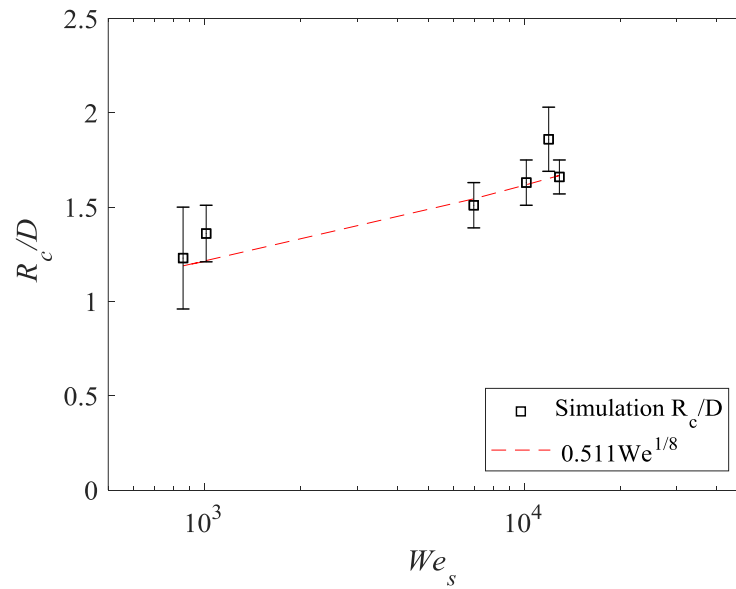
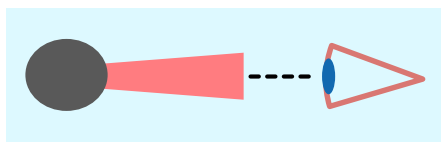
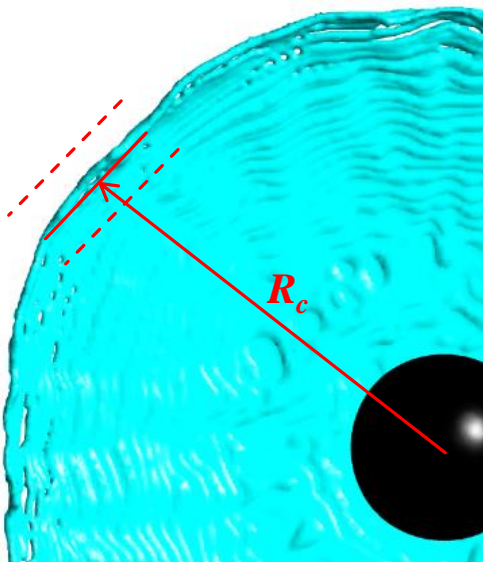
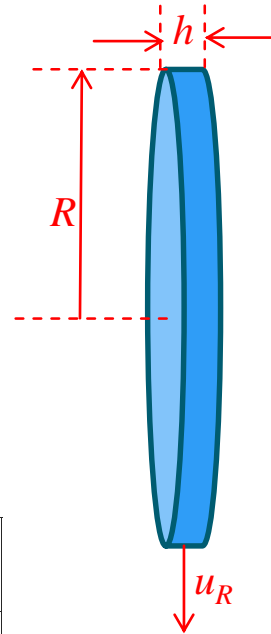
Critical Rim Radius R_c

- Splash rim radius where ligaments detach from rim
- Rim thickness approximated as h
- Criteria for ligament pinch off is $\tau_c = \tau_s$ when the capillary time of the rim matches the stretch time
- $\tau_s < \tau_c$ for the period before the rim destabilization

$$h = \frac{D^3}{6R^2}$$

$$\tau_c = \sqrt{\rho h^3 / \sigma}$$

$$\gamma = \frac{u_R}{R(t)} \quad \tau_s = 1/\gamma$$



$$R_c = 0.511 \cdot D \cdot We_s^{1/8}$$

$$We_s = \frac{\rho D u_R^2}{\sigma}$$

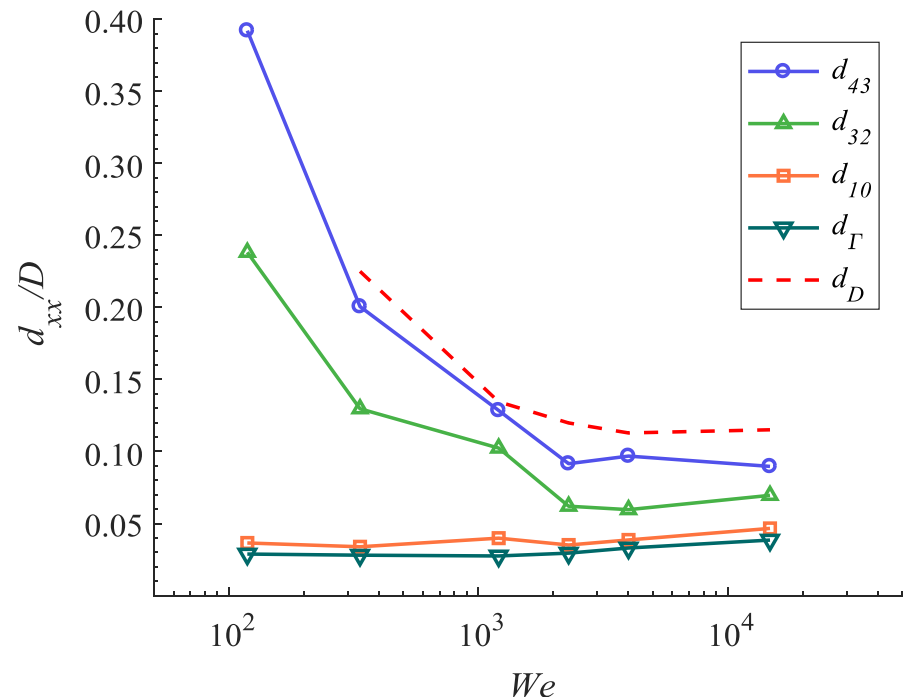
Model mean fragment diameter predictions match well with CFD simulations

- By assuming the ligament diameter is $d_L \sim h(R_c)$, the droplet diameter d_D can be approximated by the Dombrowski relation*
- For all cases the localized K value, defined as $K = Oh Re_s^{1.25}$ ranges from 400-2000
 - $d_{10}/D \sim 0.04$ is consistent with previous experiments and models for droplets impacting a solid surface** where $K \gg 58$

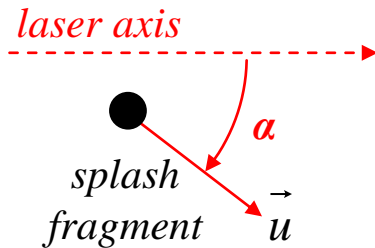
$$d_D = \left(\frac{3\pi}{\sqrt{2}} \right)^{1/3} d_L \left(1 + \frac{3\mu}{\sqrt{\rho \sigma d_L}} \right)^{1/2} \cong 1.88 d_L$$

$$d_D \approx 1.21 \cdot D \cdot We_s^{-1/4}$$

$$d_{xy} = \frac{\sum_1^N d_i^x v_i}{\sum_1^N d_i^y v_i}$$



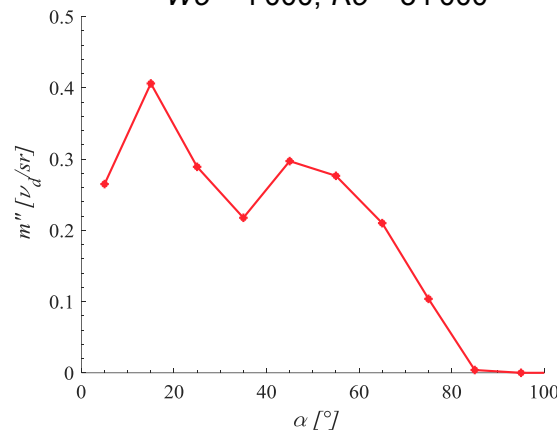
Fragment spatial distribution depends strongly on laser spot size



- Width of debris mass flux dependent on w/D
- Larger fragments distributed towards the center
- Narrowest distribution of fragments is towards the outside where the stretch is highest during breakup.

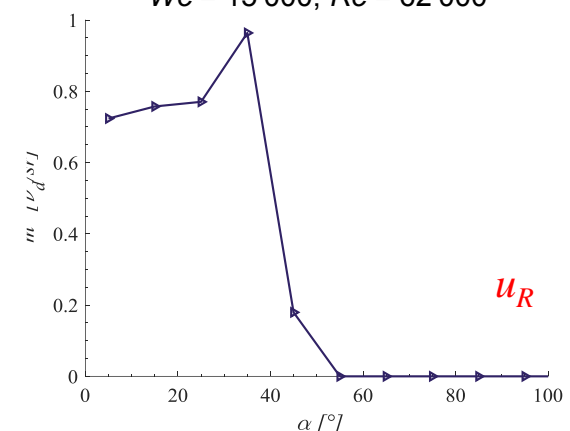
$$\frac{w}{D} = 0.41$$

$We = 4'000; Re = 34'000$

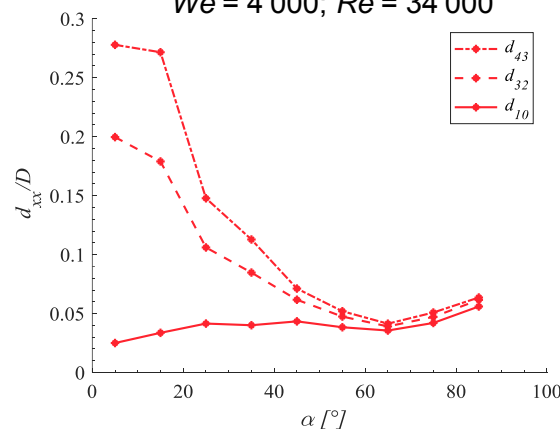


$$\frac{w}{D} = 0.97$$

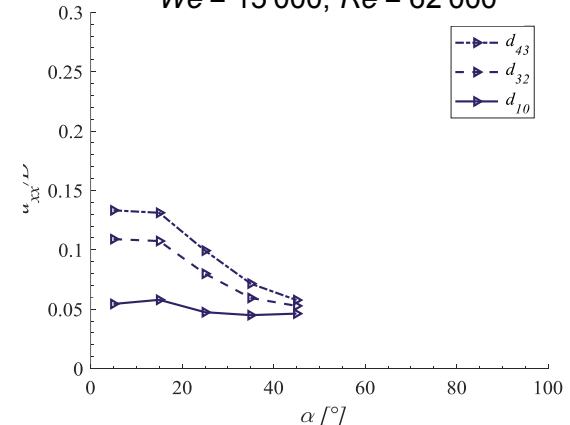
$We = 15'000; Re = 62'000$



$We = 4'000; Re = 34'000$

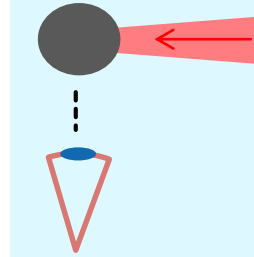


$We = 15'000; Re = 62'000$

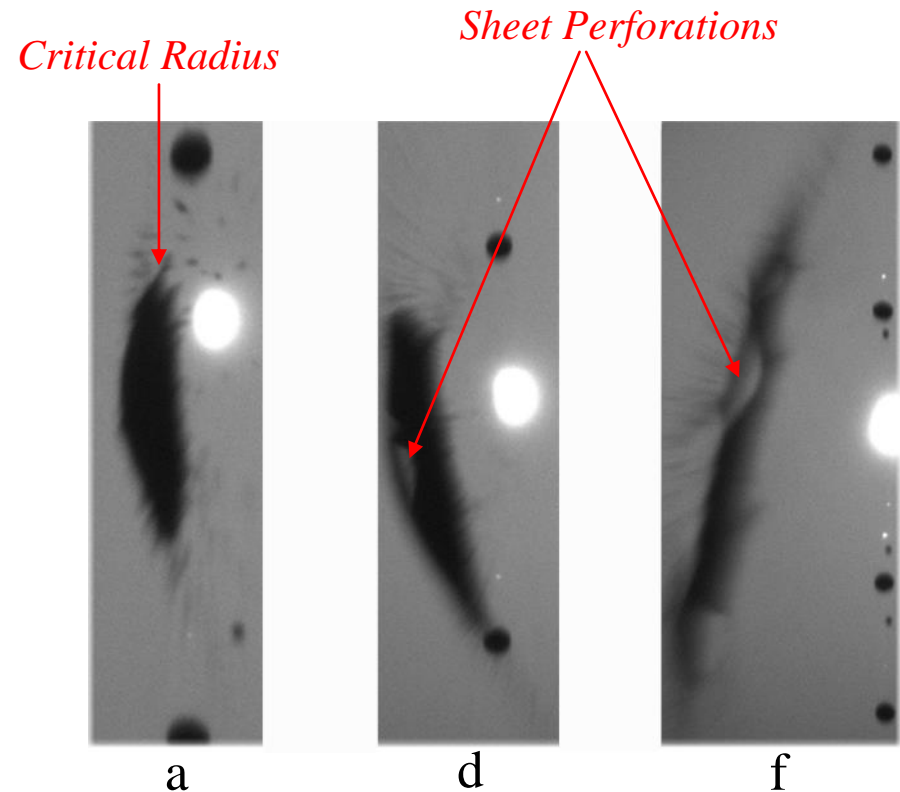


Simulation dynamics emulate phenomena observed experimentally

- Comparable cases performed experimentally*
- Critical radius is observed for lower We case
- At higher We holes are formed in middle of the sheet redistributing the stretch rate of the film



Case	a	d	f
We	80	770	3200
Re	5000	16000	32000
Oh		0.0019	
$\rho l / \rho v$		$\rightarrow \infty$	
$\mu l / \mu v$		48	
w/D		0.41	
$\log_{10}(Ep^*)$	5.4	6.1	6.7
Ee^*	78	390	1300
t^* of image		0.43	



Conclusions

- Fluent VOF CFD simulations of the droplet breakup were used to determine the fundamental mechanisms governing neutral cluster fragment size and spatial distribution
- Large velocity gradients induced in the droplet lead to a high stretch rate of the expanding droplet sheet
- As the sheet thins, capillary destabilization causes perforations to form in the sheet that grow to form ligaments that fragment into droplets
- The droplet fragments scale as $d_D \approx 1.21 \cdot D \cdot We_s^{-1/4}$
- The analytical models are tools to estimate how system parameter changes in droplet size, laser pulse energy, positional stability, etc will influence the splash flux to the ML collector
- This model can be used to help determine an optimal positional range of the ML collector mirror
- Further work will focus on determining how the droplet shape irregularities and laser alignment influence the fragment sizes and debris spatial distribution

Acknowledgments

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